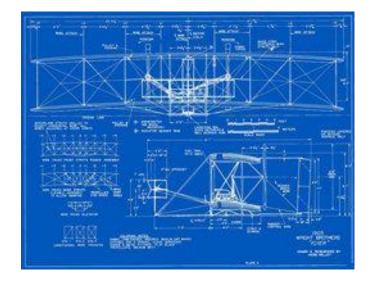


Tony Schmitz, Professor and ORNL Joint Faculty University of Tennessee, Knoxville



We live in a digital world





is now...

What was once blueprints and pencils

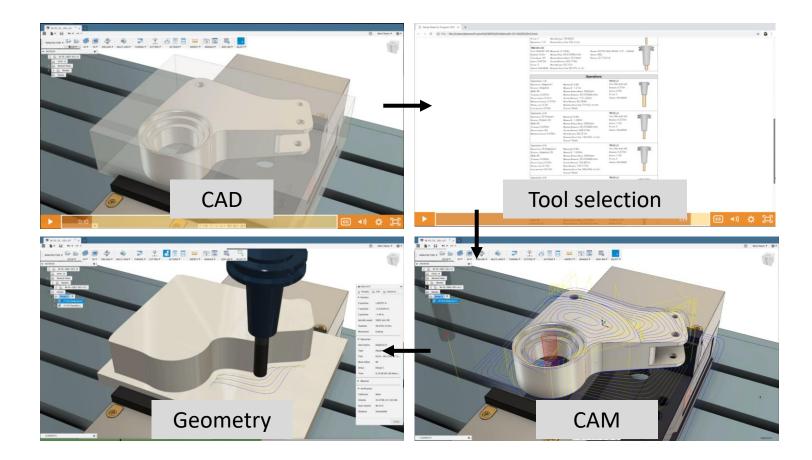


solid models and software applications.

We live in a digital world

For discrete part manufacturing by machining, the digital world steps are:

- Design the part using computer-aided design (CAD) software
- Select the cutting tools that will be used to remove material from the pre-form (bar stock, forging, casting, additively manufactured near-net shape part)
- Generate the tool path using computeraided manufacturing (CAM) software to produce the final design from the preform
- Remove material by following the tool path
- Inspect the part for conformance to design specifications (geometry, surface finish, microstructure, ...)



What can go wrong?

These steps suggest that a digital world treatment is sufficient, but we live in a physical world. What can go wrong?

EBZC

The tool may not follow the commanded path

- machine tool positioning errors
 - quasi-static kinematics/thermal state
 - dynamic high-speed contouring

The tool may wear out

- Machining is a competition between the sharp cutting edge and workpiece
- Higher speeds lead to higher temperature and accelerated wear
- Empirical tool material/geometry, work material, coolant, parameters (sub-optimal)

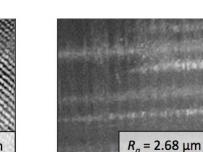
Vibration may be excessive

- The cutting force causes tool/workpiece displacement
- Can result in chatter, a self-excited vibration
- Behavior depends on setup (sub-optimal)

Machine tool may fail

- Preventative maintenance
- Predictive maintenance













Let's consider vibration implications

400

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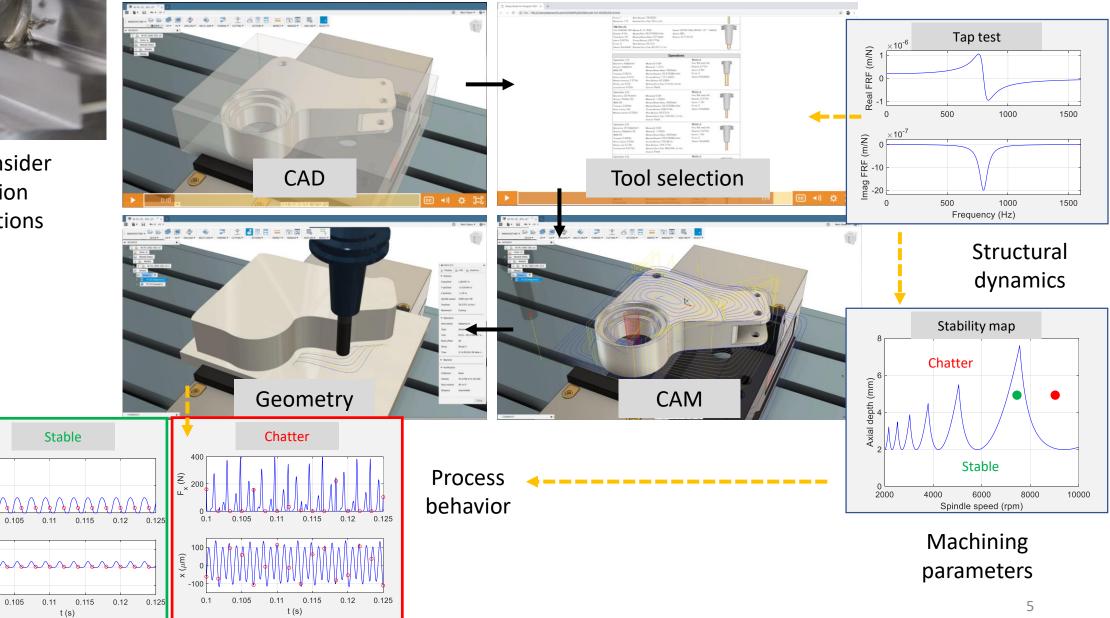
100 (µ7/) ×

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Ê 1. 200

Machining is more than geometry





Let's consider vibration implications

400

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100 (µ7/) ×

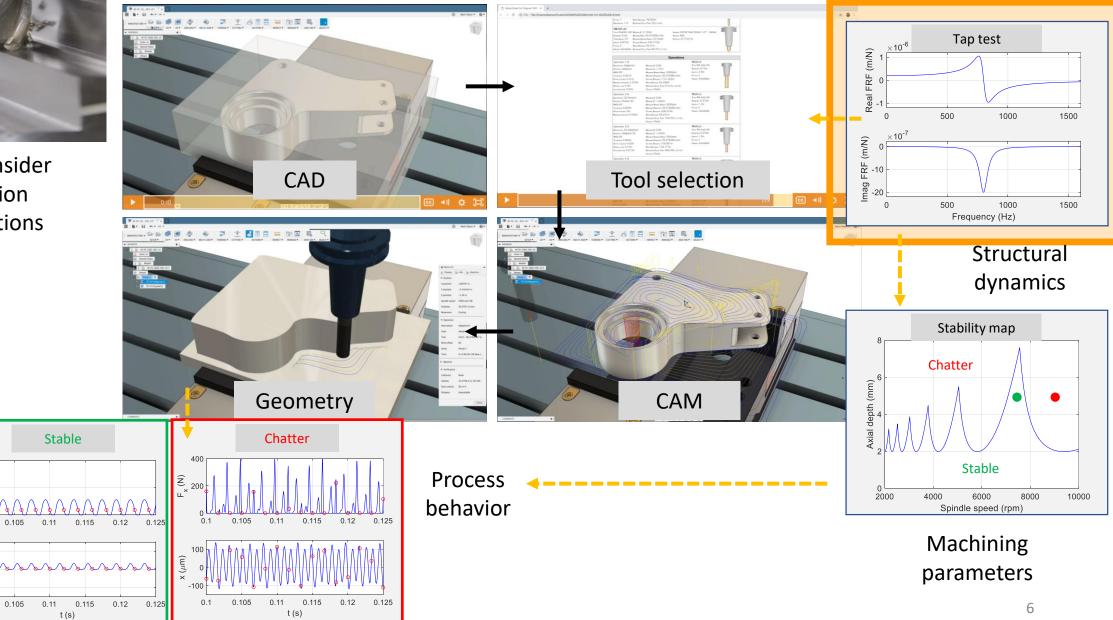
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Machining is more than geometry



All structures vibrate

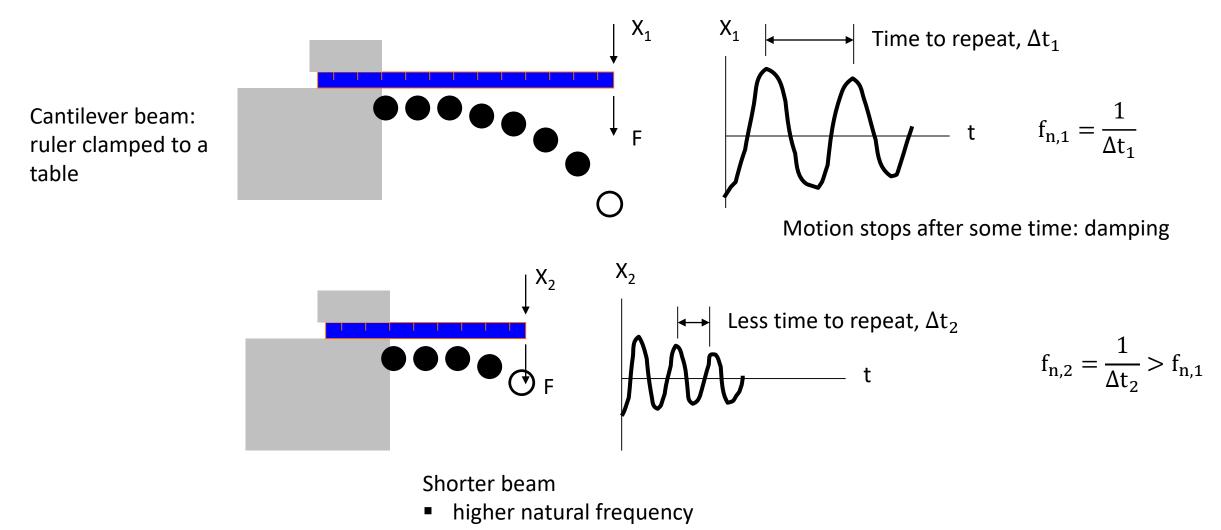






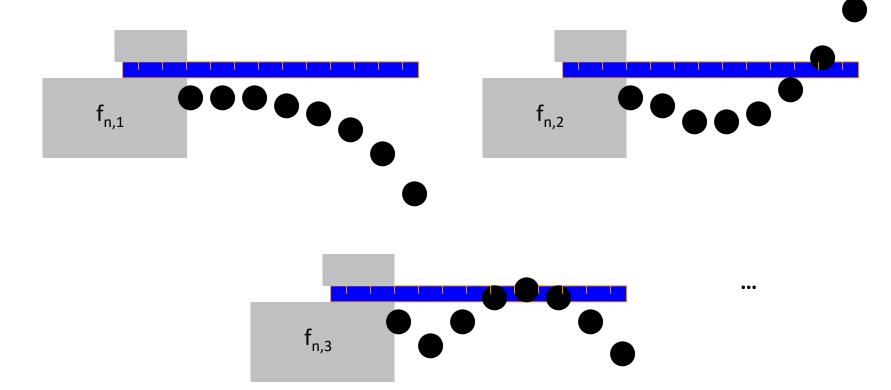


Natural frequency: vibrating frequency that is inherent to the structure



smaller amplitude for same excitation; it has higher stiffness

- Mode shape: deformation profile while vibrating at a natural frequency
- Cantilever beam 1st, 2nd, and 3rd mode shapes
- Each mode shape has an associated natural frequency

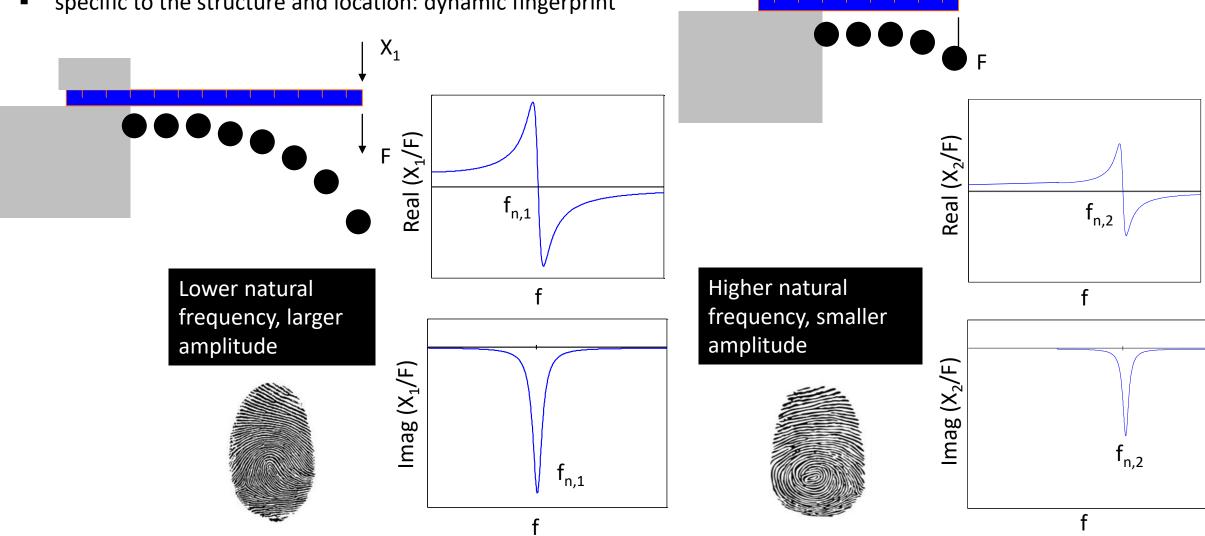


Multiple natural frequencies and associated mode shapes are present in every structure.

 X_2

Frequency response function (FRF)

- contains information about natural frequency, stiffness, and damping
- specific to the structure and location: dynamic fingerprint



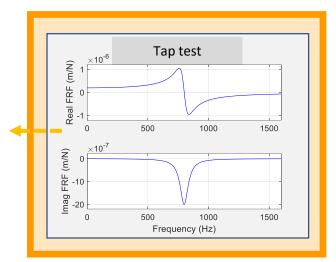
Larger amplitude **Frequency response function (FRF)** can be expressed mathematically with smaller stiffness Excitation complex-valued function (real and imaginary parts) and damping frequency Real (X/F) $\operatorname{Re}\left[\frac{X}{F}(f)\right] = \frac{1}{k} \left(\frac{1 - \left(\frac{f}{f_n}\right)}{\left(1 - \left(\frac{f}{f_n}\right)^2\right)^2 + \left(2\zeta\left(\frac{f}{f_n}\right)\right)^2}\right)$ Stiffness f_n **Damping ratio** Natural frequency Imag (X/F) $\operatorname{Im}\left[\frac{X}{F}(f)\right] = \frac{1}{k} \left(\frac{-2\zeta \frac{f}{f_n}}{\left(1 - \left(\frac{f}{f_n}\right)^2\right)^2 + \left(2\zeta \left(\frac{f}{f_n}\right)\right)^2}\right)$ f_n

f

Tap test

- Instrumented hammer excites the structure
- Accelerometer measures the response
- Ratio is the FRF
- Provides the information required to predict machining performance







Let's consider vibration implications

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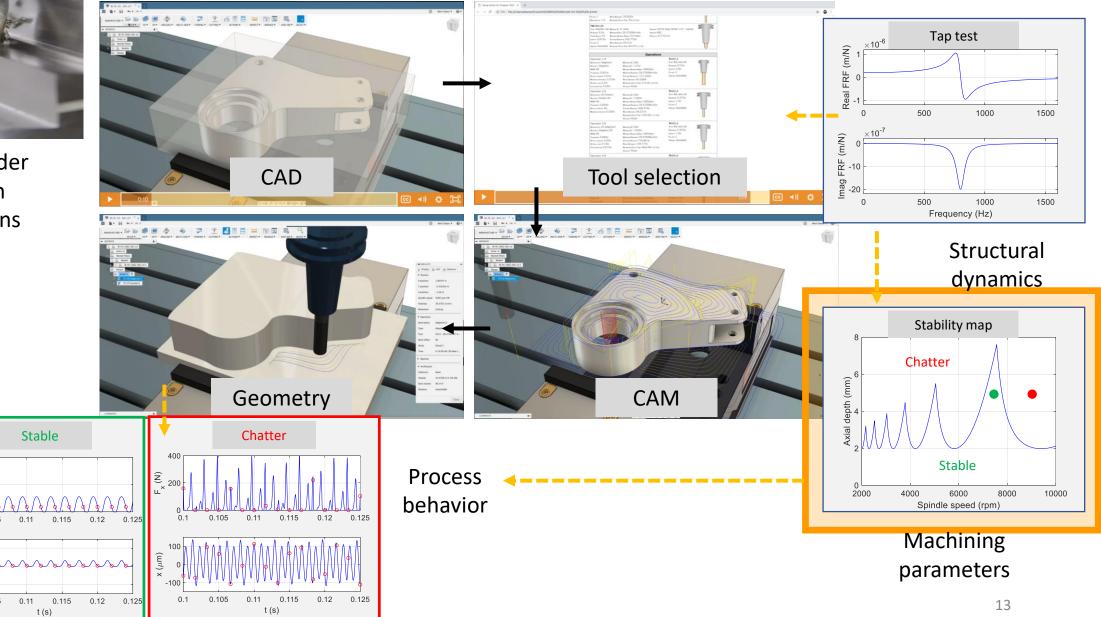
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Machining dynamics



Tool flexibility

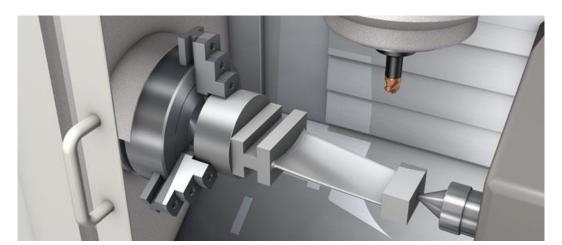
Cutting tools are designed to be stiff. The materials are selected to be hard and resist deformation.

However, when the cutting force is applied to the tool it still deflects. You can think of a tool as a stiff spring.

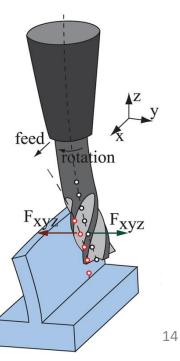


Workpiece flexibility

Sometimes the workpiece is also flexible. In this case, the workpiece can deflect as much or more than the tool when the cutting force is applied. It can also be thought of as a spring.

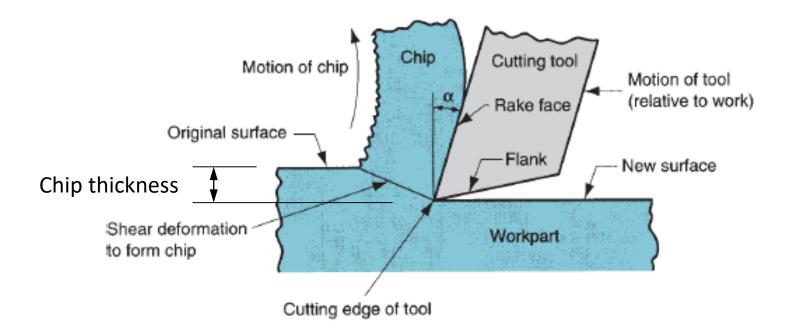


Damping is also important!



Cutting force

The cutting force is generated as the tool shears away material in the form of a chip.

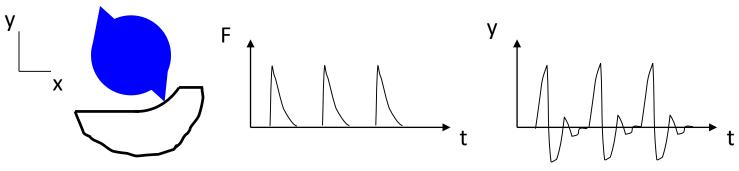


- The cutting force depends on the chip thickness, chip width (into page), material properties, and tool geometry.
- Larger chip width/thickness and gives higher force.

Why does vibration occur in milling?

- teeth constantly enter and exit the cut
- the cutting force varies with these entries and exits
- the variable cutting force acts on the flexible tool and/or workpiece and causes displacement
- this variable displacement is vibration
- the amplitude of vibration depends on the tool/workpiece stiffness and spindle rotating frequency



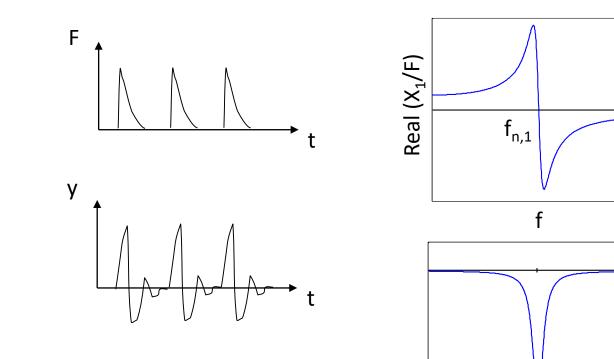


There are two main types of vibration in milling.

1) Forced vibration

The variable force causes the tool or workpiece to vibrate at the same frequency. For a spindle speed of 12000 rpm and a cutter with two teeth, the tooth passing frequency is 12000/60*2 = 400 Hz.

The corresponding amplitude of vibration depends on the relationship between the tooth passing frequency and the tool/workpiece dynamics. We describe the dynamics using the **frequency response function**, or FRF.



f_{n,1}

f

2) Self-excited vibration

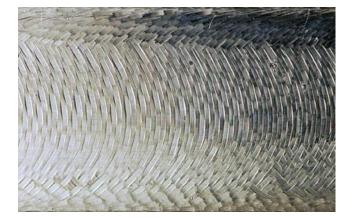
Steady input force is modulated into vibration at the system **natural frequency**.

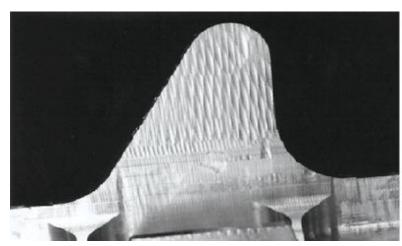
Examples include:

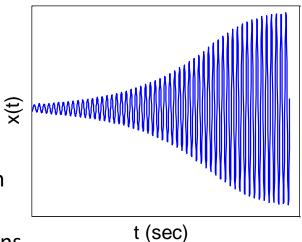
- whistle steady air flow produces acoustic vibration
- violin bow across string produces vibration at frequency that depends on the string length
- airplane wing flutter
- chatter in machining steady excitation of teeth impacting work leads to large tool vibrations at system natural frequency



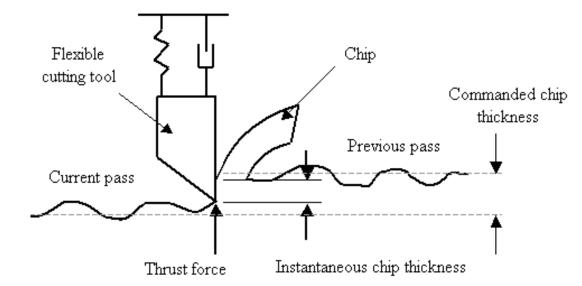
Tacoma Narrows Bridge opened in July 1940, but collapsed due to aero-elastic flutter four months later.





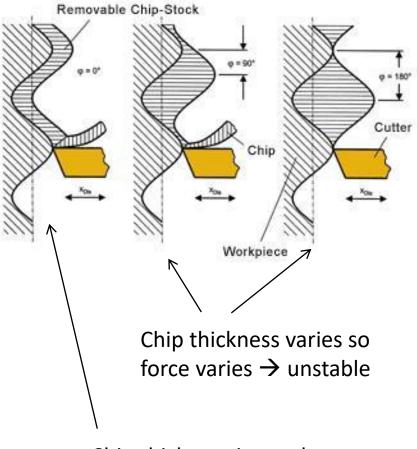


Why does chatter (self-excited vibration) occur in machining?



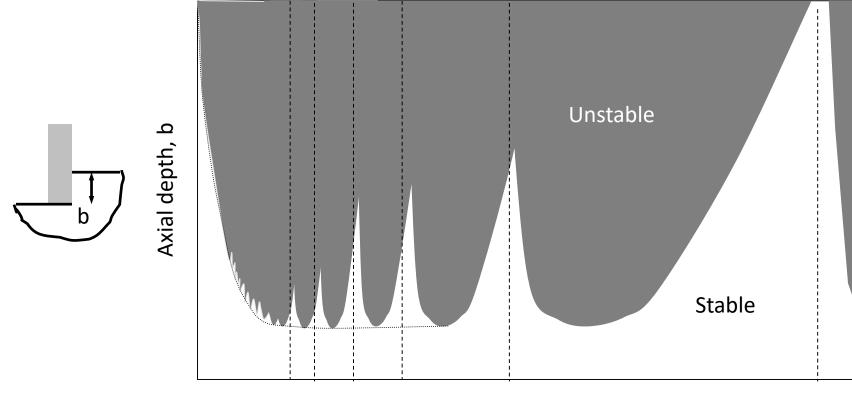
Regeneration is a primary mechanism for chatter

- force depends on chip thickness
- chip thickness depends on current vibration and previous pass
- current vibration depends on force



Chip thickness is nearly constant – small force variation \rightarrow stable

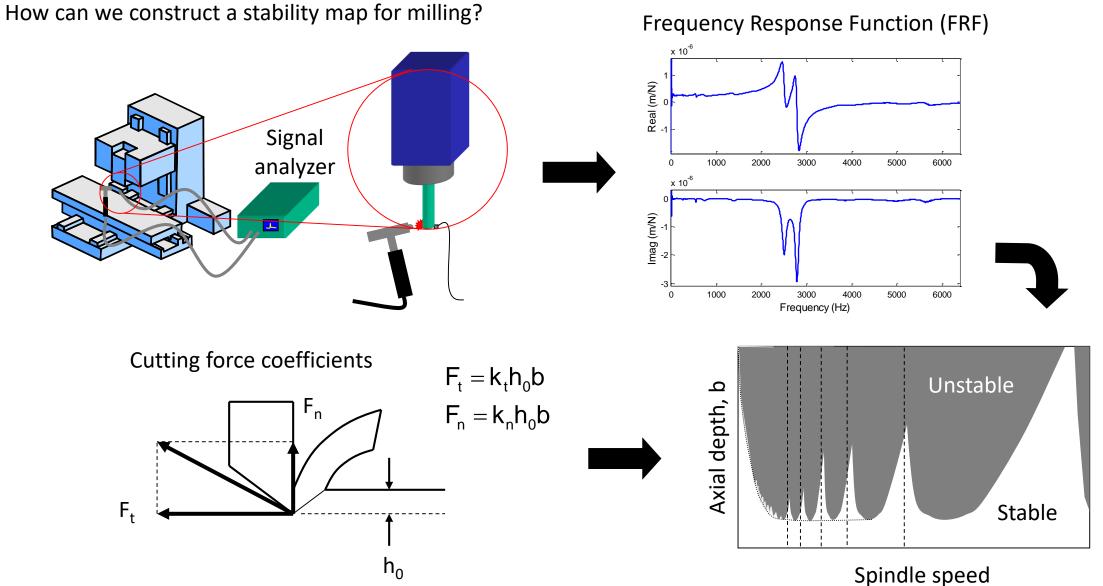
feedback



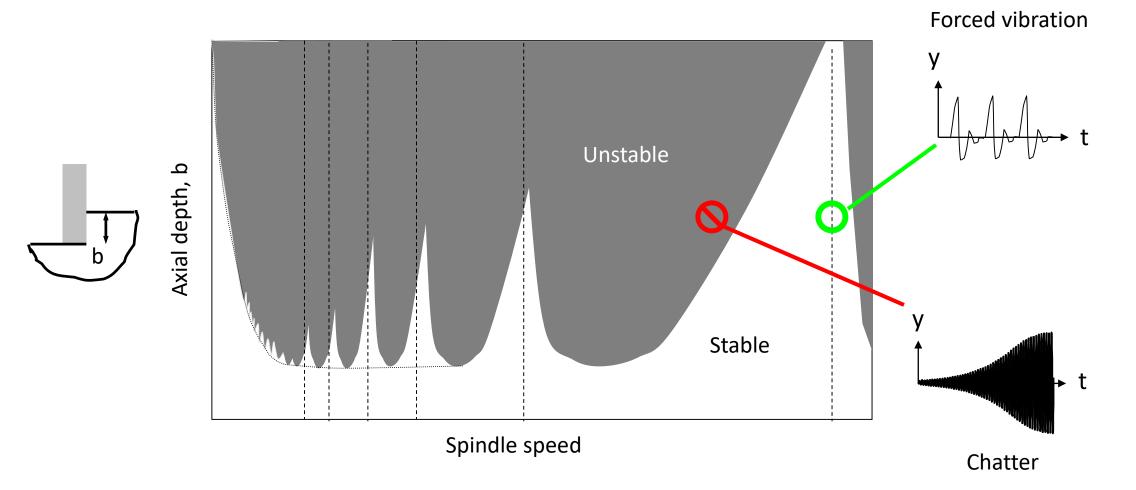
Spindle speed

Stability map for milling

- separates unstable (chatter) from stable (forced vibration) zones
- select spindle speed and axial depth combination to obtain stable cutting conditions without trial cuts
- best spindle speeds depend on dynamics and probably do not correspond to handbook values.



How do the two vibration types relate to the stability lobe diagram?





Let's consider vibration implications

400

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100 (m⁷¹) x

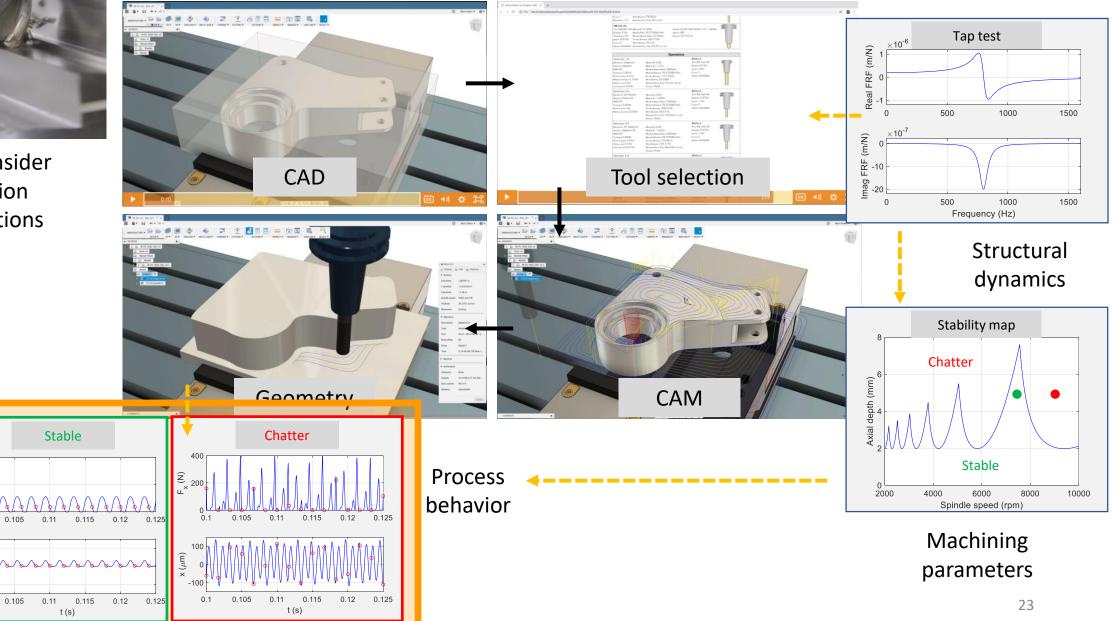
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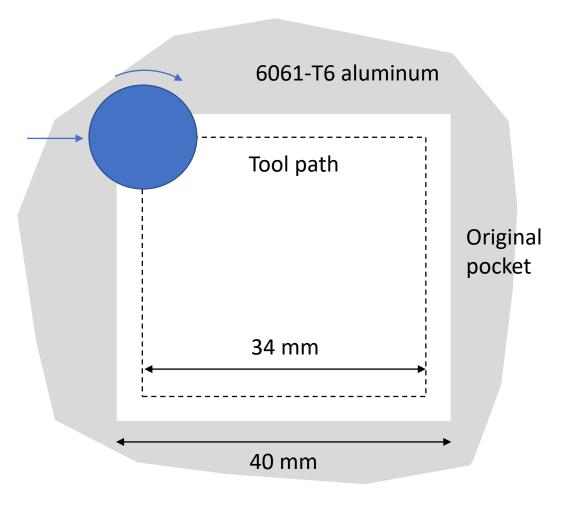
Ê., 200

Machining dynamics



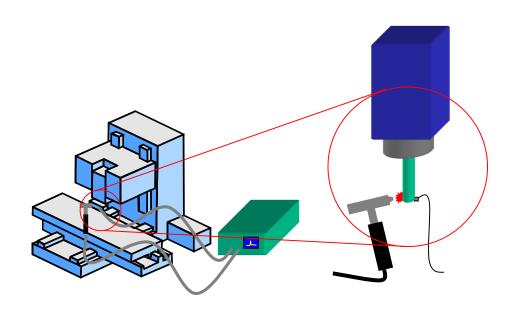
Test case description

- 25% radial immersion up milling (3 mm radial depth)
- 12 mm diameter endmill, 4 teeth, 30 deg helix
- 4 mm axial depth
- 0.25 mm feed per tooth
- {5500, 6400, 7400} rpm spindle speed

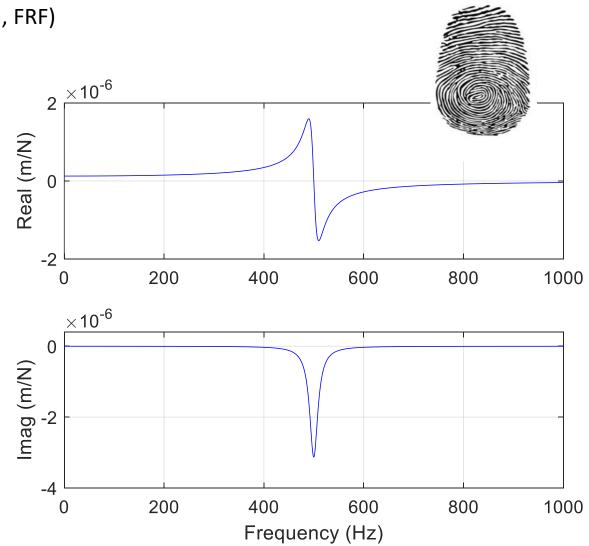


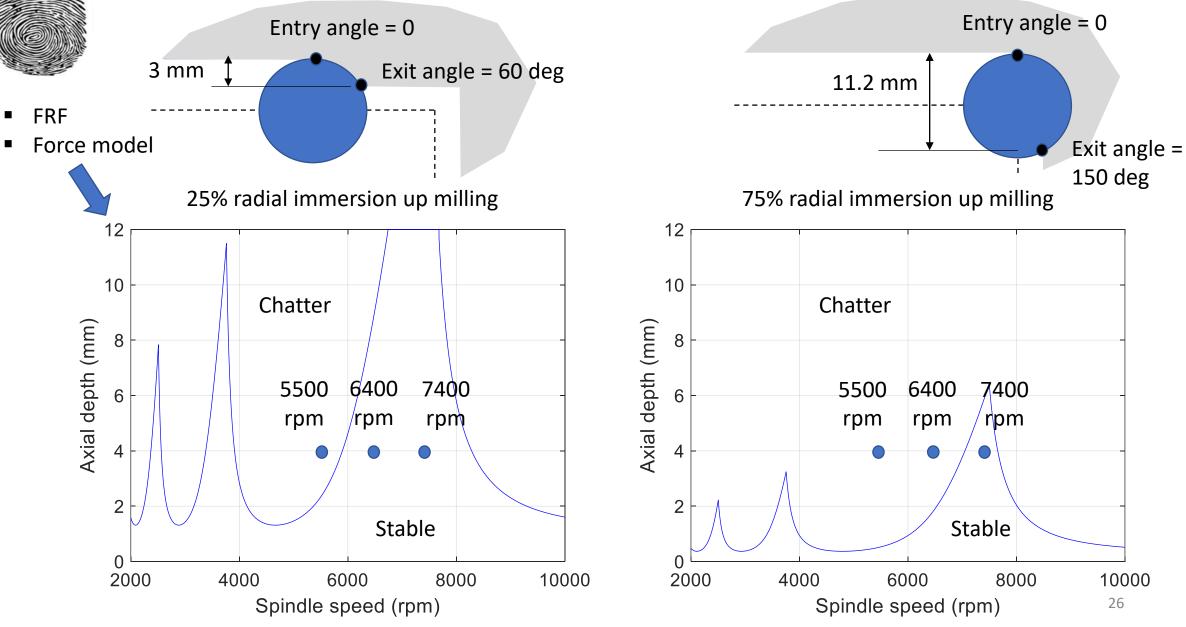
Tool point dynamic response (frequency response function, FRF)

- 500 Hz, 8×10⁶ m/N stiffness, 2% damping
- x (feed) and y directions assumed symmetric
- workpiece assumed rigid relative to tool



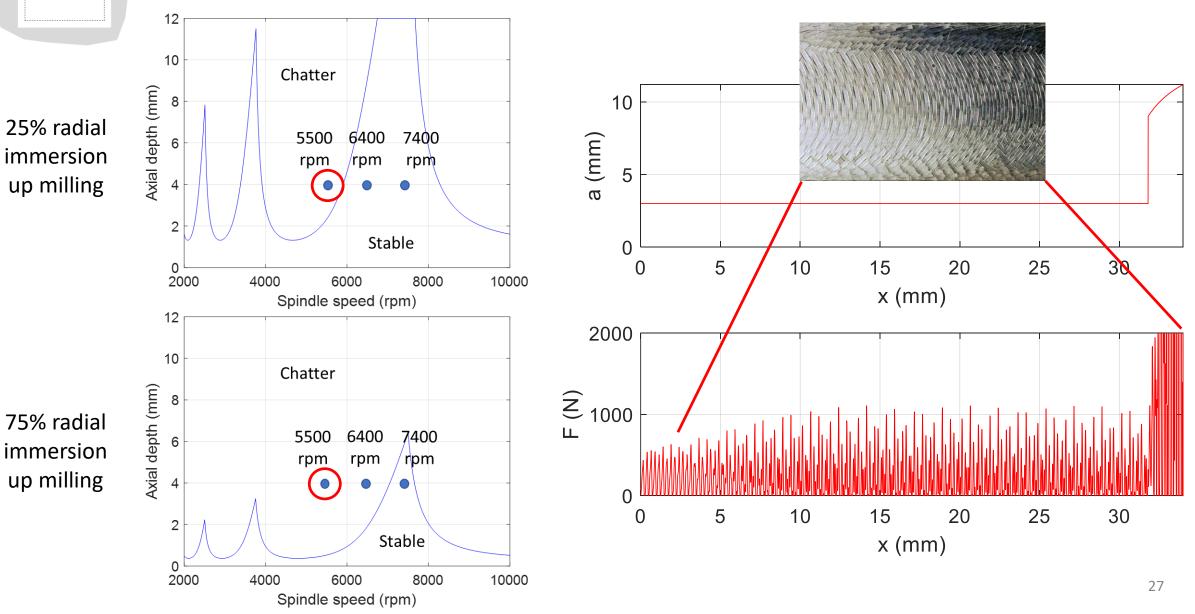
Cutting force model: 6061-T6 aluminum





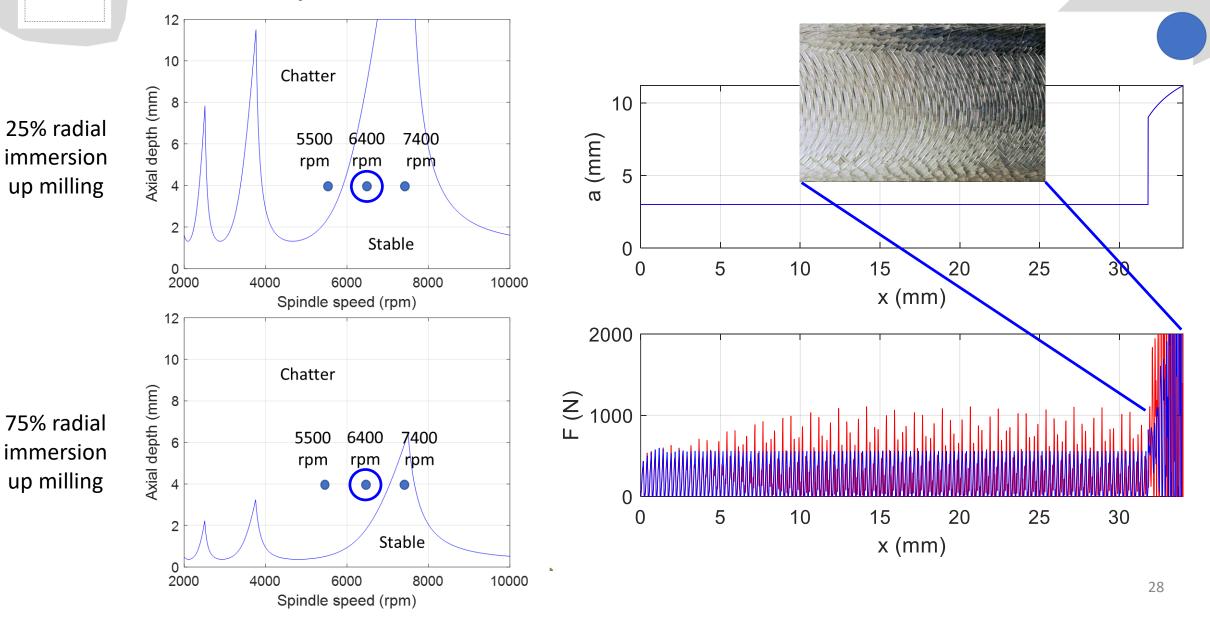
5500 rpm: Unstable for 25% radial immersion, unstable for 75% radial immersion

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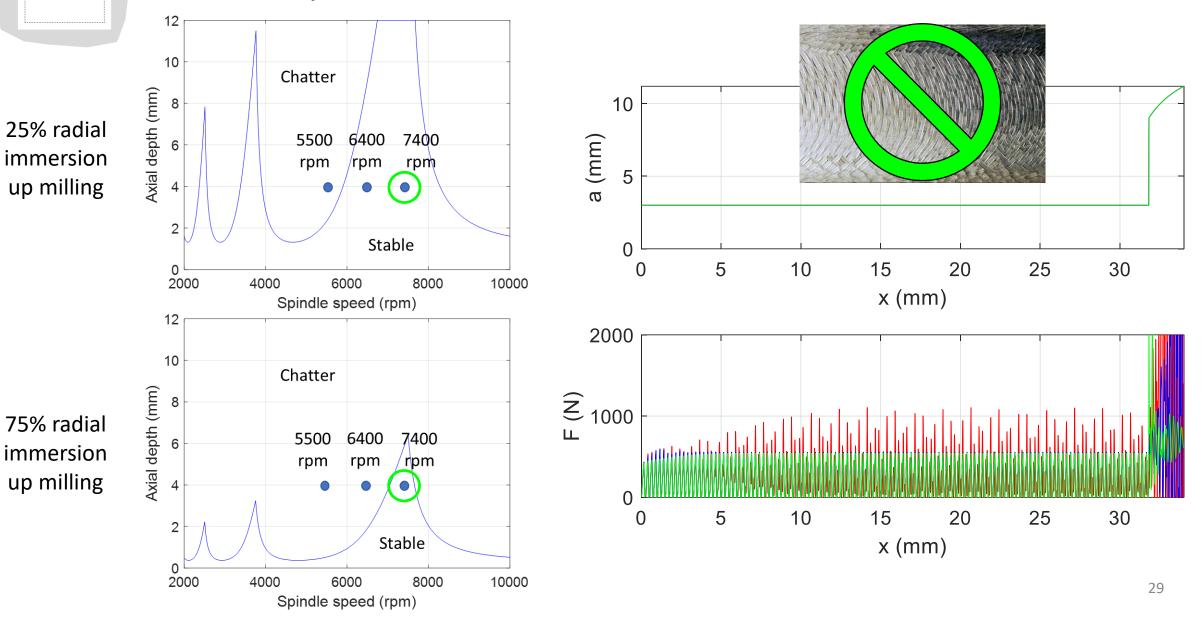
6400 rpm: Stable for 25% radial immersion, unstable for 75% radial immersion

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7400 rpm: Stable for 25% radial immersion, stable for 75% radial immersion

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400

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100 (m4) ×

-100

0.1

0.1

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Machining is more than geometry

